# CIFellows 2020-2021

Computing Innovation Fellows

## Surface wind stress model for turbulent flows above ocean surface waves

Kianoosh Yousefi and Marco Giometto

Department of Civil Engineering and Engineering Mechanics, Columbia University

#### Introduction

- About **two-thirds** of the surface of the Earth is covered by the **ocean**.
- The air-sea exchanges of mass, momentum, and energy over such a huge area play an integral role in determining the **sea state**, **weather patterns**, and **climate** and thus significantly <u>impact many</u> aspects of human life.
- Although we know that surface waves are critically important, we do not yet fully understand the <u>fundamental physics of ocean waves</u>.
- The current parameterizations of air-sea fluxes are limited, and that prevents us from, for example, making accurate predictions of extreme wind events such as tropical storms and hurricanes.
- The objective of this study is to develop an accurate wall-layer model for use in large-eddy simulations (LESs) that capture the salient features of air-sea fluxes.

#### Large-eddy simulation of wind field

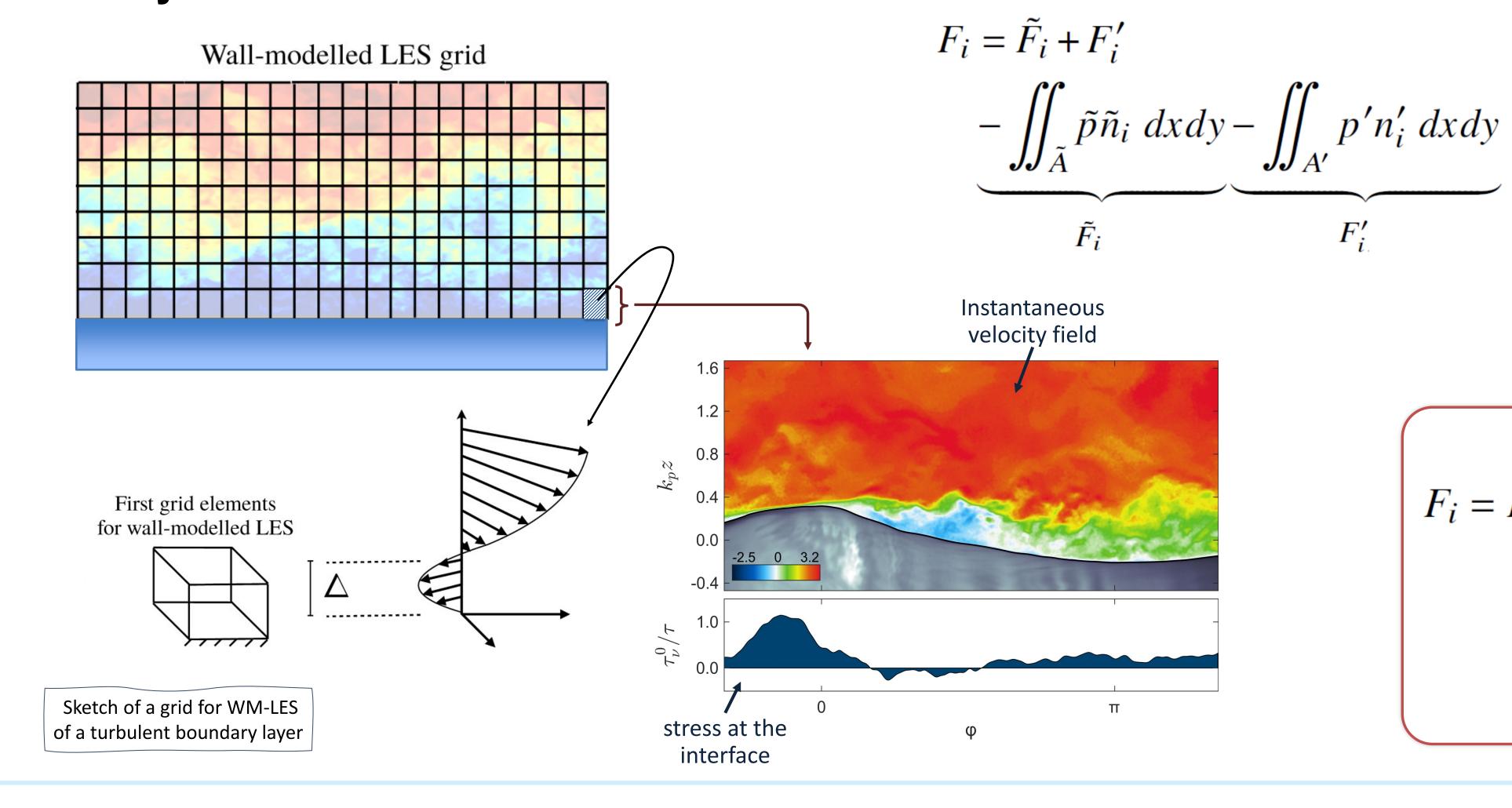
$$\frac{\partial \tilde{u}_{i}}{\partial x_{i}} = 0$$

$$\frac{\partial \tilde{u}_{i}}{\partial x_{i}} + \tilde{u}_{j} \left( \frac{\partial \tilde{u}_{i}}{\partial x_{j}} - \frac{\partial \tilde{u}_{j}}{\partial x_{i}} \right) = -\frac{1}{\rho} \frac{\partial \tilde{p}}{\partial x_{i}} - \frac{\partial \tau_{ij}}{\partial x_{j}} + \frac{1}{\rho} \delta_{i1} \Pi + F_{i}$$

Here,  $\tilde{u}$  is the filtered (or resolved) velocity, u' is the residual (sub-grid scale) component,  $\tau_{ij}$  is the SGS stress tensor,  $F_i$  is a body force, and  $\Pi$  is the streamwise pressure gradient driving the flow:

$$\frac{1}{\rho}\Pi = -\frac{u_*^2}{L_z}$$
 friction velocity height of the computational domain

### Wall-layer model for sea surface stress



$$\begin{cases} \widetilde{F}_{i} = -\rho \iint_{A} C_{D}\widetilde{u}_{i}R\left(\widetilde{u}_{r,j}\frac{\partial\eta}{\partial x_{j}}\right) dxdy \\ \longrightarrow C_{D} \approx \left(\kappa \ln^{-1}\frac{\delta_{z}}{\alpha_{w}\sigma_{\eta}^{\Delta}}\right)^{2} \end{cases}$$

$$F'_{i} = -\rho \iint_{A} \left[\frac{\kappa}{\log(\delta_{z}/\alpha_{w}\sigma_{\eta}^{\Delta})}\right]^{2} \|\widetilde{\boldsymbol{u}}_{r}\|\widetilde{u}_{r,i} dxdy$$

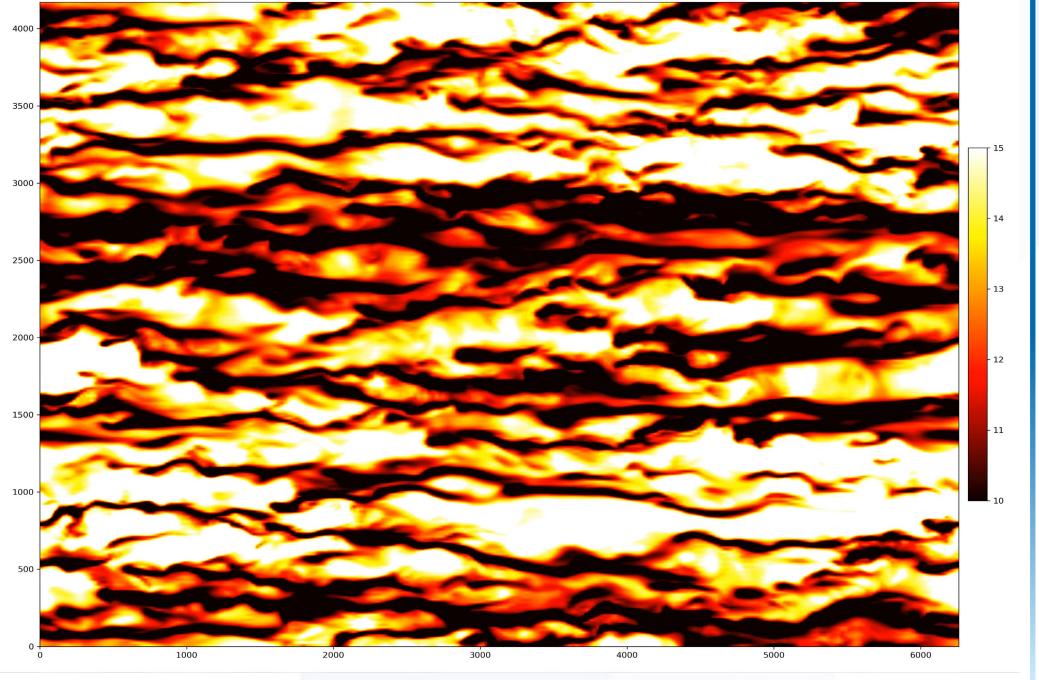
$$F_{i} = \tilde{F}_{i} + F'_{i} = -\rho \iint_{A} \left( \kappa \ln^{-1} \frac{\delta_{z}}{\alpha_{w} \sigma_{\eta}^{\Delta}} \right)^{2} \tilde{u}_{i} R \left( \tilde{u}_{r,j} \frac{\partial \eta}{\partial x_{j}} \right) dx dy$$

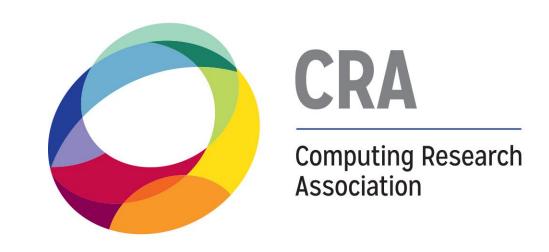
$$-\rho \iint_{A} \left[ \frac{\kappa U_{r}(x, y, \delta_{z})}{\log \left( \delta_{z} / \alpha_{w} \sigma_{\eta}^{\Delta} \right)} \right]^{2} \frac{\tilde{u}_{r,i}(x, y, \delta_{z})}{U_{r}(x, y, \delta_{z})} dx dy$$

#### Scale invariant constraint

The <u>scale invariant constraint</u> requires the total **drag force** to be **independent of the resolution**. Thus, we dynamically obtain the drag by filtering  $F_i$  equation at two different filter scales: one is the LES filter scale of  $\Delta$  and the other is a test-filter scale of  $a\Delta$ , where a > 1.

$$F_i = \tilde{F}_i + F_i' = \tilde{\tilde{F}}_i + \tilde{F}_i'$$
 filtering at scale  $\Delta$  scale  $2\Delta$ 









\* This is the current state of our work, with the underlying theory finalized. Additional processing and analysis of the results are ongoing.

